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(71) Applicant(s):
Visteon Global Technologies, Inc.
(Incorporated in USA - Michigan)
Intellectual Property Department,
One Village Center Drive,
Van Buren Township, MI 48111,
United States of America

(72) Inventor(s):
GuomIng George Zhu
Kevin David Moran

(74) Agent and/or Address for Service:
Dummett Copp
25 The Square, Martlesham Heath,
IPSWICH, Suffolk, IP5 3SL,
United Kingdom

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(54) Abstract Title: **Methods of Diagnosing Open Secondary Winding of an Ignition Coil using the Ionization Current Signal**

(57) The invention relates to detecting an open secondary winding of an ignition coil of an internal combustion engine ignition system. In one embodiment, an open secondary winding is detected by enabling an integrator, resetting the integrator, detecting an ionization current, integrating the ionization current over a spark window, comparing the integrated ionization current with a threshold, and setting an open secondary flag if the integrated ionization current is below the threshold. In another embodiment, an open secondary winding is detected by measuring spark duration. This may involve comparing an ionization signal with a first threshold, measuring the spark duration when the ionization signal is greater than the first threshold, comparing said spark duration with a second threshold, and setting an open secondary flag.

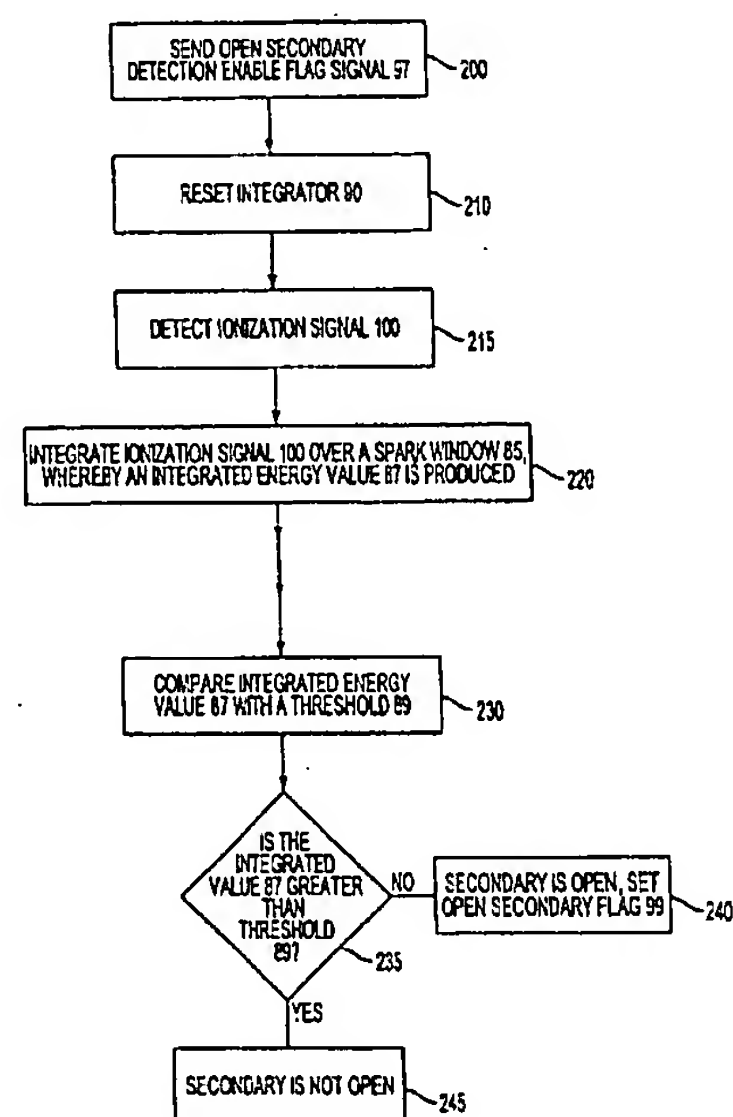


FIG. 7

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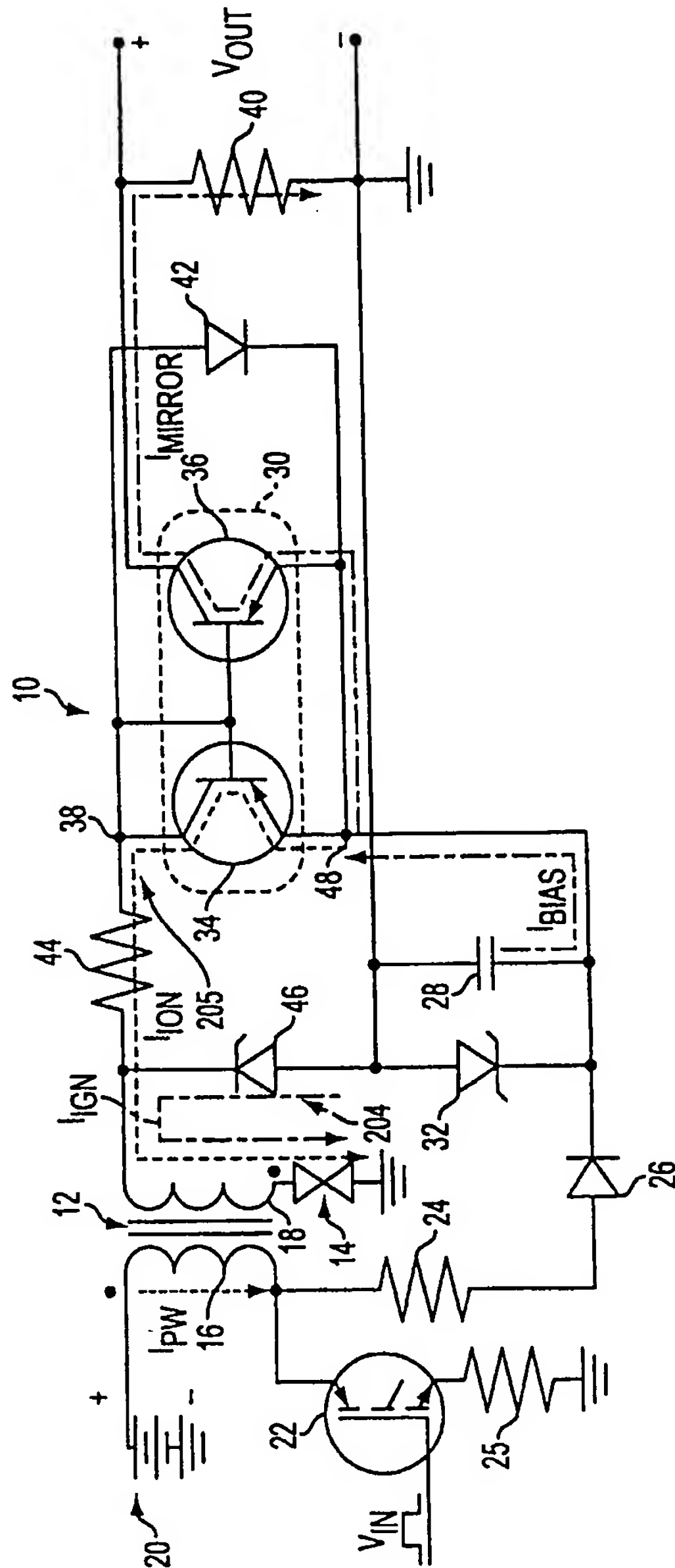


FIG. 1

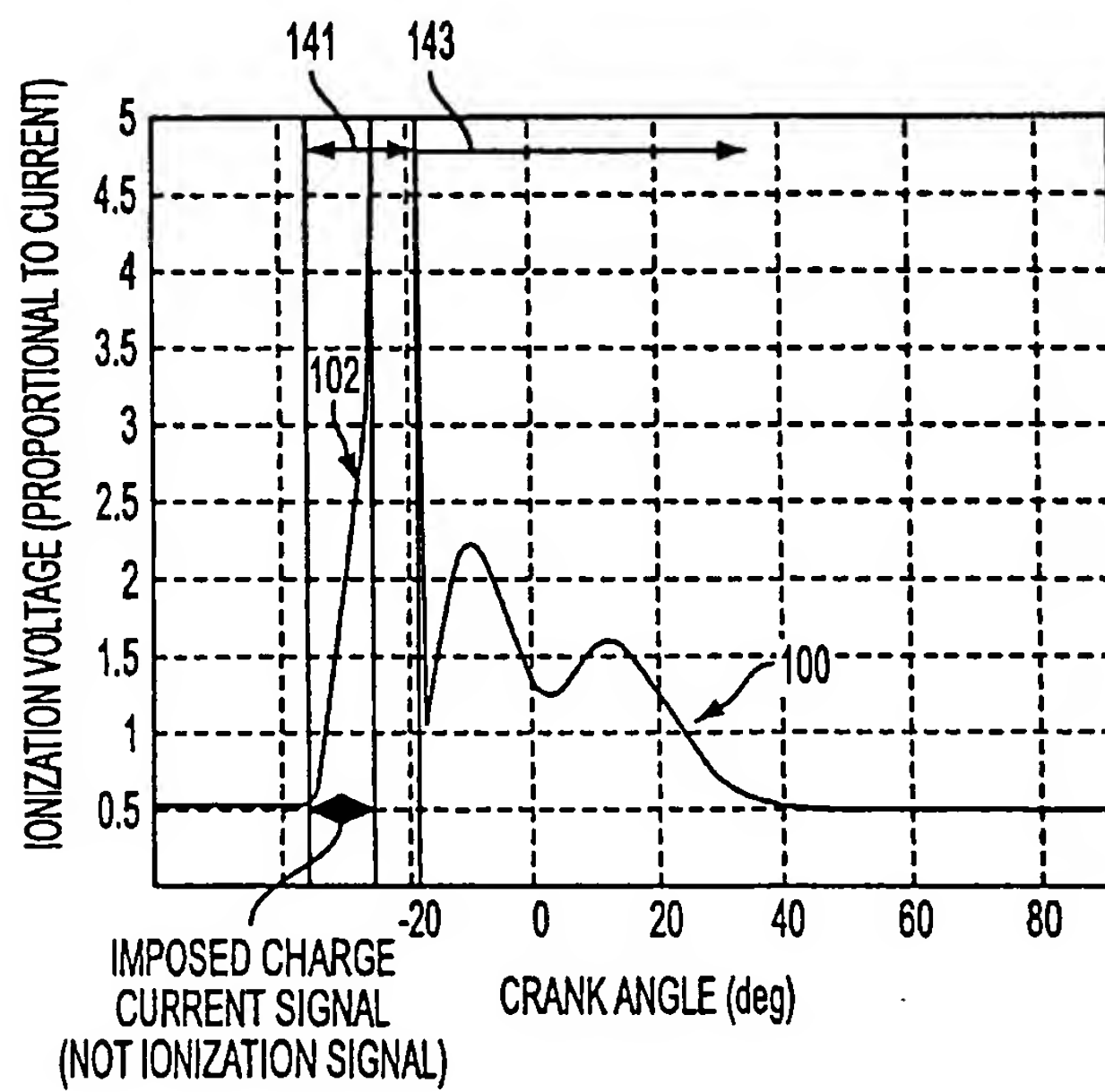


FIG. 2

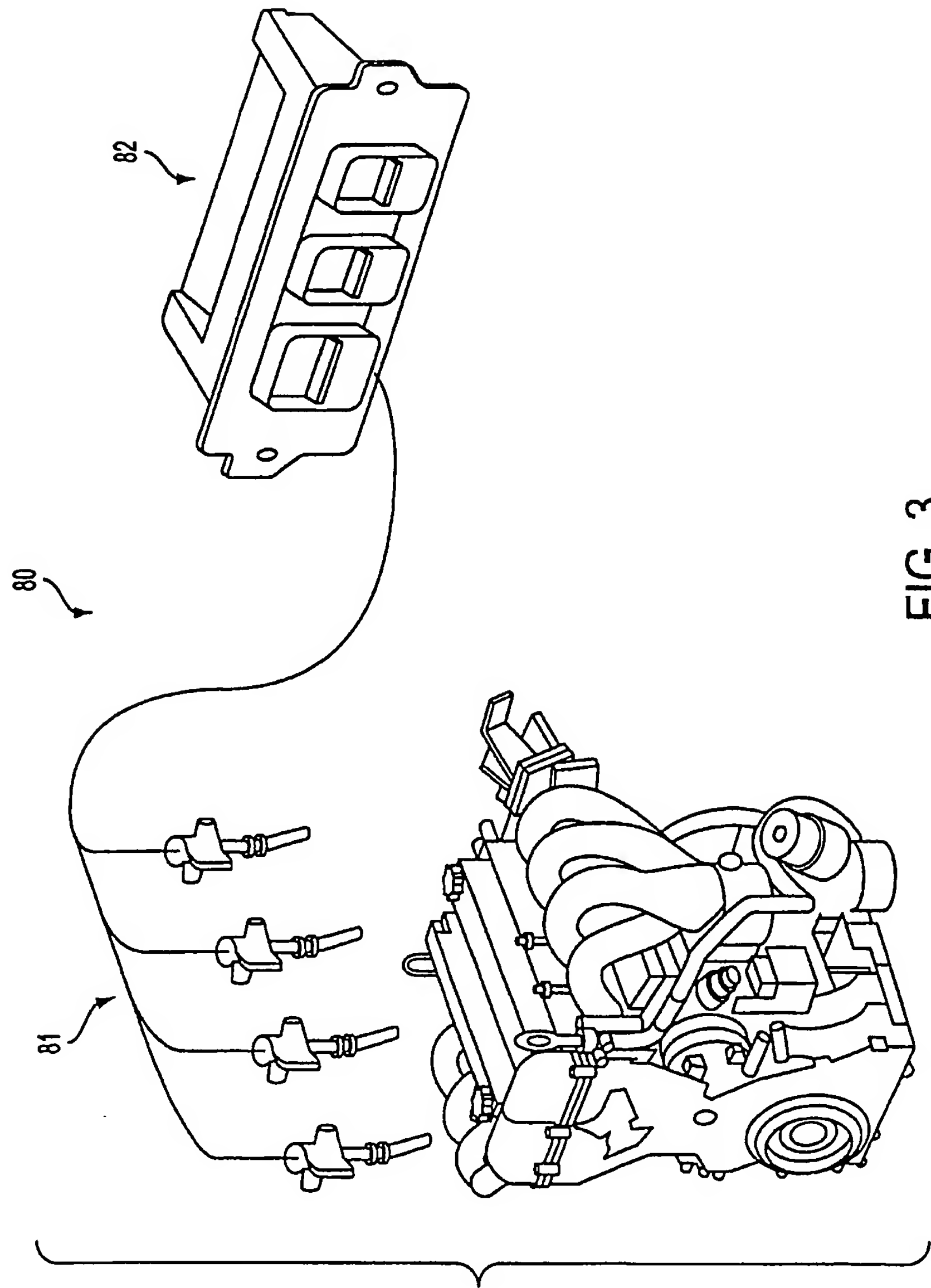


FIG. 3

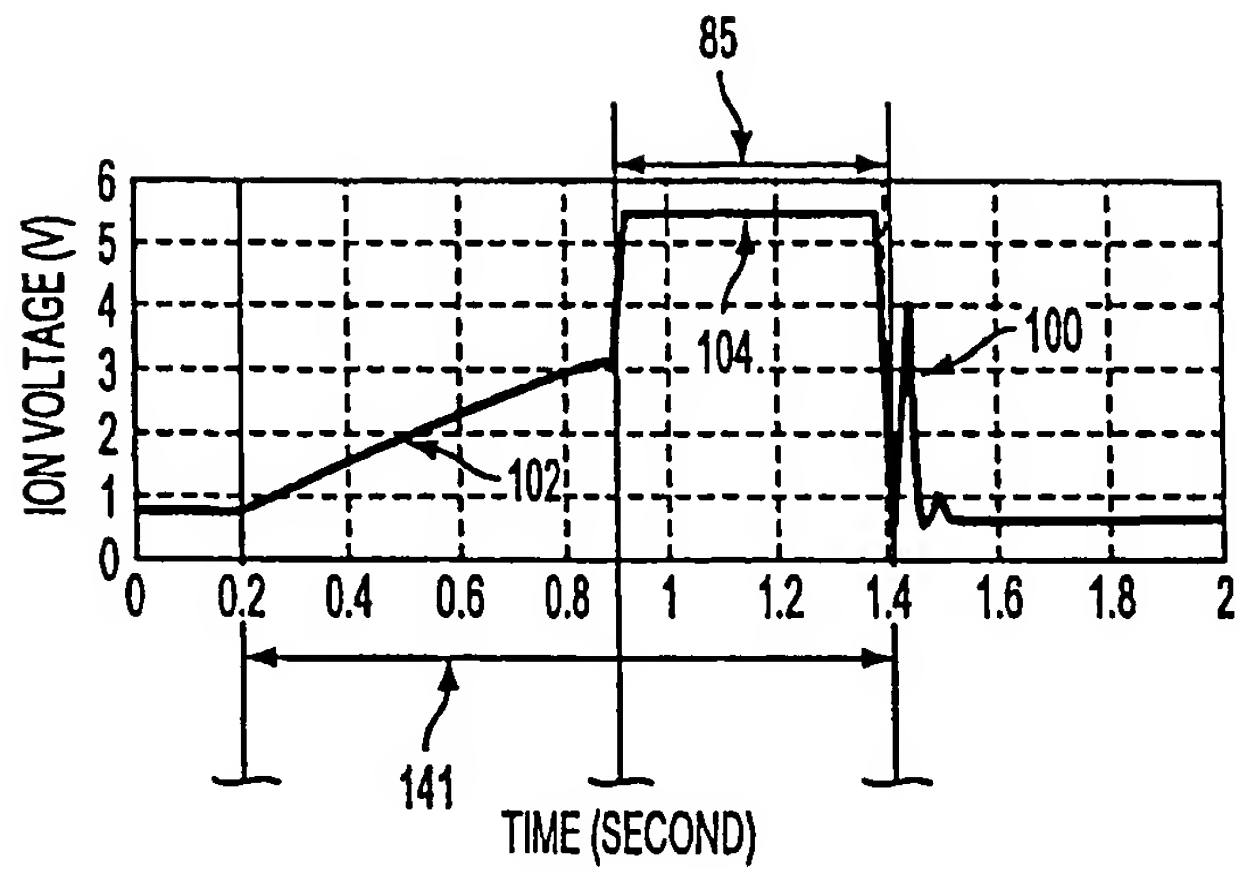


FIG. 4a

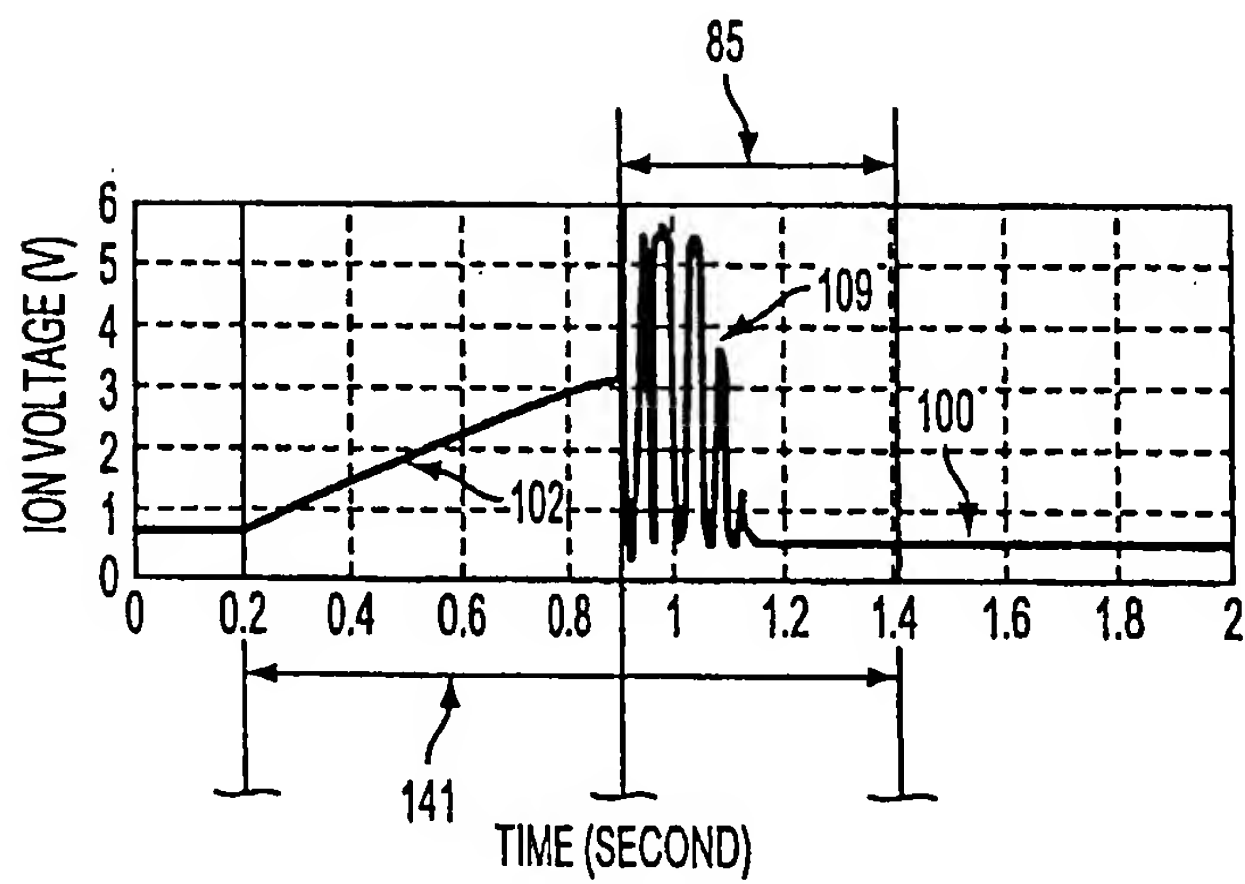


FIG. 4b

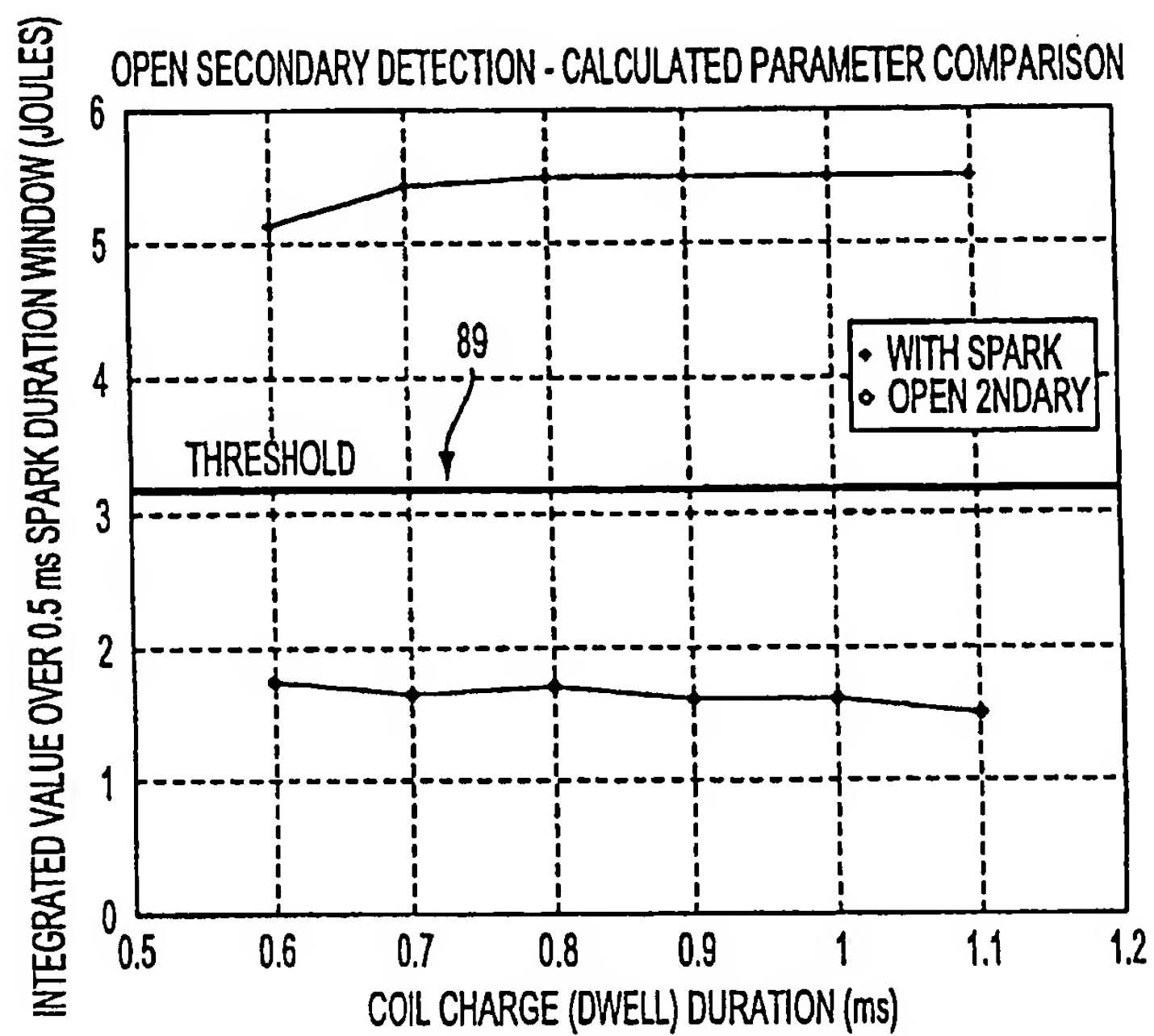


FIG. 5

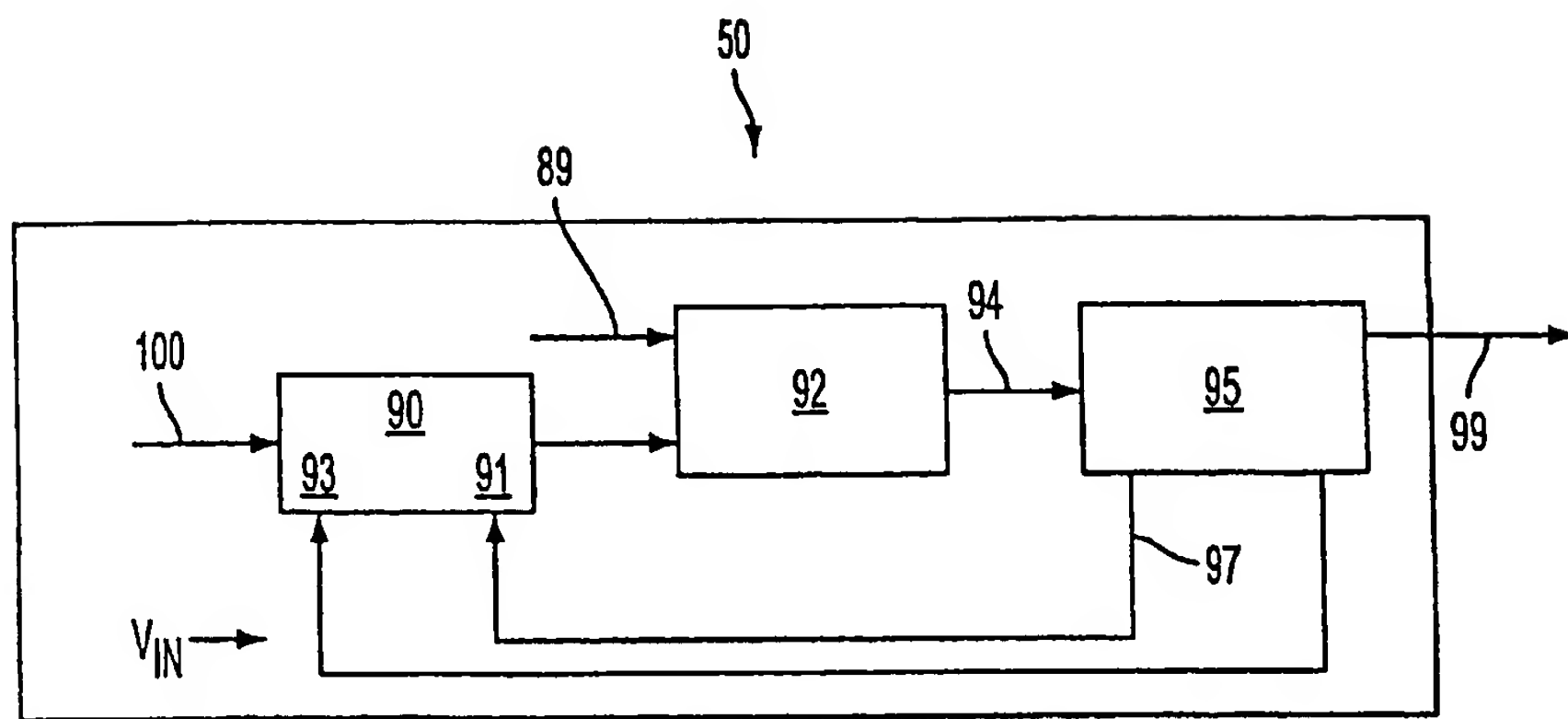


FIG. 6

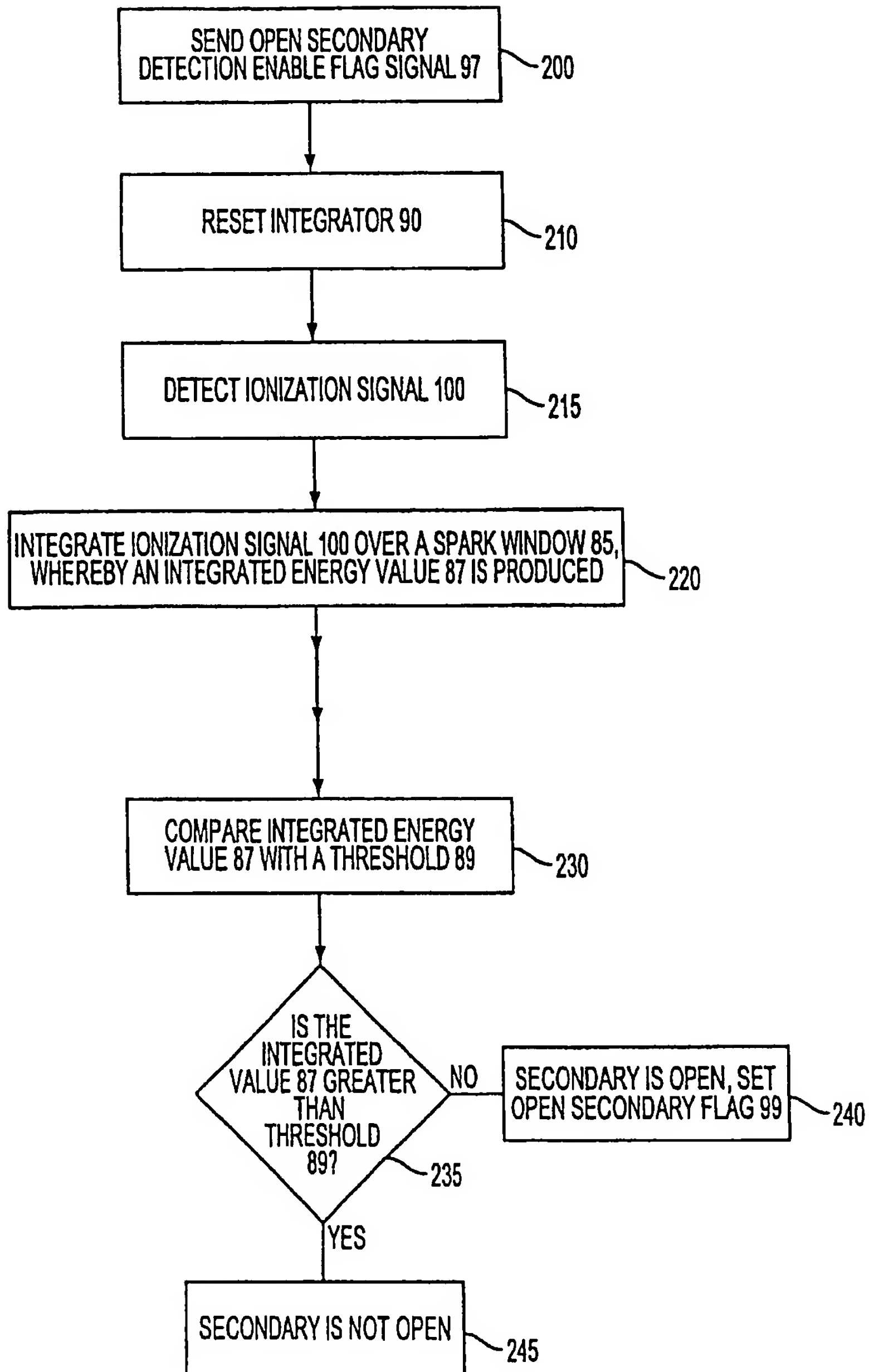


FIG. 7

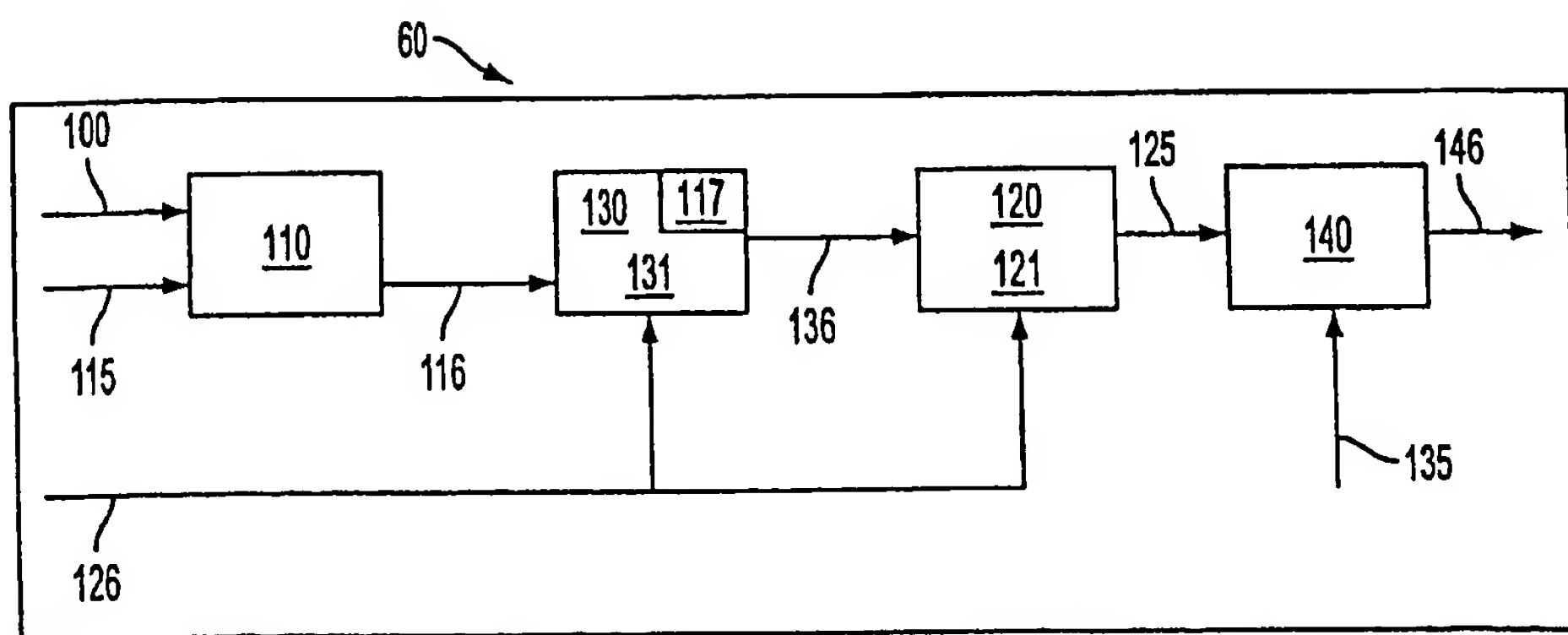


FIG. 8

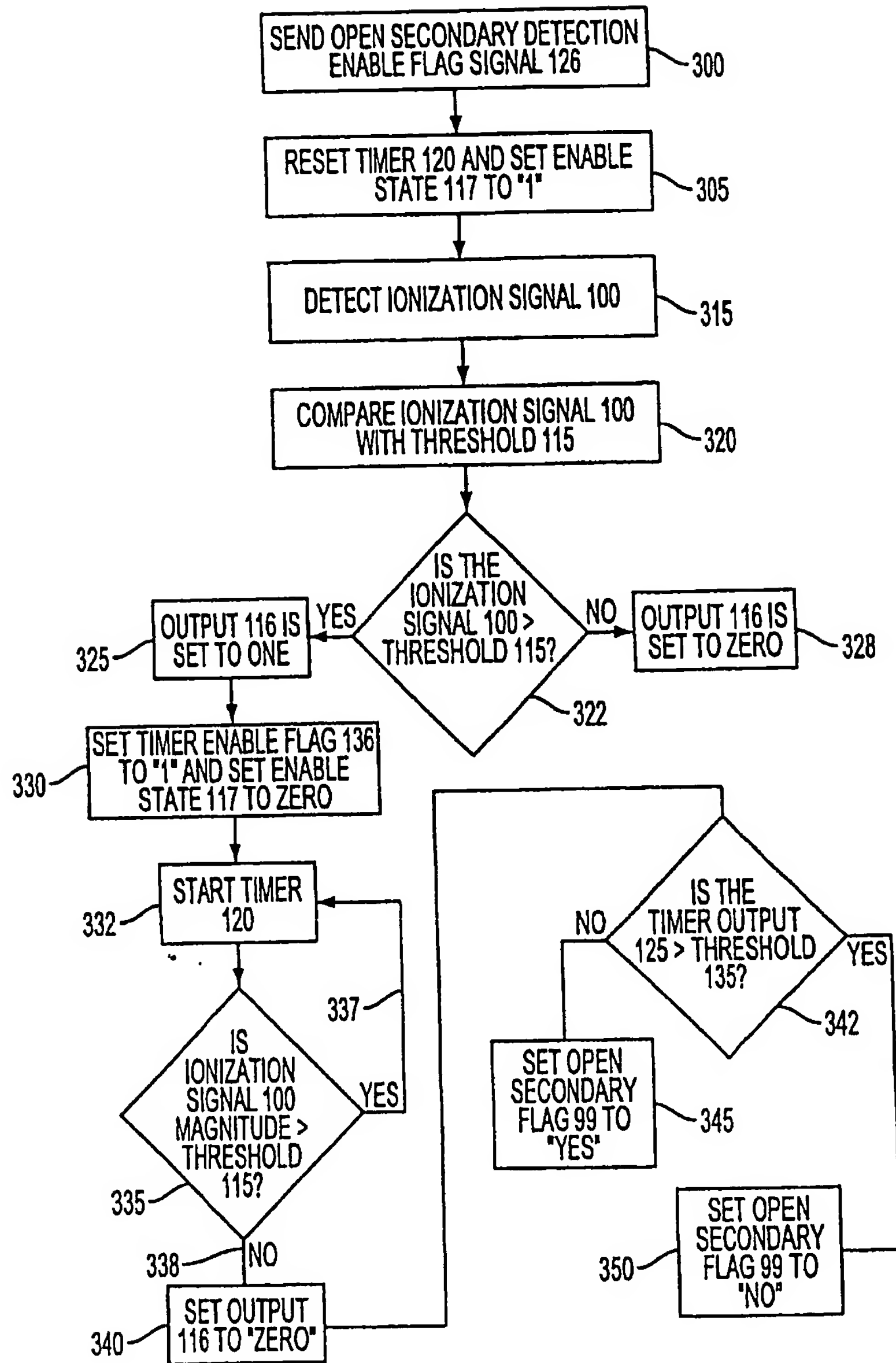


FIG. 9

Methods of Diagnosing Open-Secondary Winding of an Ignition
Coil Using the Ionization Current Signal

Background of the Invention

5

1. Technical Field

This invention is related to the field of internal combustion
(IC) engine ignition systems. More particularly, it is
10 related to the field of detecting an open secondary winding
of an ignition coil.

2. Discussion

15 Typically, an ignition coil and an ignition or a spark plug
are disposed in a combustion chamber of an internal
combustion engine. The ignition coil includes a primary
winding and a secondary winding. The ignition plug is
connected in electrical series between a first end of the
20 secondary winding and ground potential. If the spark plug is
not connected (as is the case where the secondary is open),
no spark will be generated, and part of the charged energy is
dissipated through ringing current caused by capacitance
between the secondary winding and ground. Since the charged
25 energy is not dissipated by a spark, the fly-back energy
dissipated by the IGBT over the primary winding side after
the end of charge is much higher than the case when the
secondary winding is connected to a spark plug and a spark
occurred after the coil was charged. In fact, the total
30 energy dissipated by the IGBT connected to the ignition coil
with an open secondary winding could be as great as four
times more than when the secondary winding is connected to a

spark plug. This indicates that the heat dissipation of the IGBT could be four times more than the normal operational condition. A heat sink is required to protect the IGBT from being overheated for both normal operational and open
5 secondary conditions. This increases cost of the ignition system. However, in some cases the open-secondary condition may be prevented.

Summary of the Invention

10

The failure of a spark plug to spark is reflected in the ionization signal. Since there is no ignition current in the case of an open-secondary winding, an open secondary winding can be detected by observing whether a spark occurred.

15

According to the invention, there is provided a method of detecting an open secondary winding in a motor vehicle spark ignition system, comprising the steps of:

- enabling an integrator;
- 20 resetting said integrator;
- detecting an ionization voltage;
- integrating said ionization voltage over a spark window;
- comparing said integrated ionization voltage with a threshold; and
- 25 setting an open secondary flag if said integrated ionization voltage is below said threshold.

Also according to the invention, there is provided a method of detecting an open secondary winding in a motor vehicle
30 spark ignition system, comprising the step of measuring spark duration.

The invention further provides an open secondary winding detection apparatus for a motor vehicle spark ignition system, comprising:

5 a first comparator having a first and a second input and an output, wherein said first input is operably connected to an ionization signal and said second input is operably connected to a first threshold;

10 a controller having a first and an enable input and an output, wherein said first input is operably connected to said output of said first comparator;

a timer having a first and an enable input, and an output, wherein said first input is operably connected to said output of said controller; and

15 a second comparator having a first and a second input and an output, wherein said first input is operably connected to said output of said timer and said second input is operably connected to a second threshold.

20 In a preferred embodiment, the step of enabling an integrator comprises sending an open secondary detection enable flag signal to an enable input of the integrator.

The invention additionally provides an open secondary winding detection apparatus for a motor vehicle spark ignition system, comprising:

25 an integrator having an ionization signal input, an enable input, a reset input and an output; and

30 a comparator having a first input operably connected to said output of said integrator, a second input operably connected to a threshold value, and an output.

In another preferred embodiment, the step of measuring spark

duration comprises the steps of comparing an ionization
signal with a first threshold, measuring the spark duration
when the ionization signal is greater than the first
threshold, comparing the spark duration with a second
5 threshold, and setting an open secondary flag.

In a further preferred embodiment, the step of measuring
spark duration comprises the steps of detecting an ionization
signal over a spark window, comparing the ionization signal
10 with a first threshold, enabling a timer if the detected
ionization signal is greater than the first threshold,
disabling the timer after the detected ionization signal
falls below the first threshold, comparing the timer's output
with a second threshold, and setting an open secondary flag
15 if the timer's output is below the second threshold.

In another preferred embodiment, the open secondary winding
detection apparatus further comprises a powertrain control
module having an input operably connected to the output of
20 the comparator and an output operably connected to the enable
input of the integrator, whereby an open secondary detection
enable flag signal is sent by the powertrain control module
to the enable input of the integrator, and wherein the reset
input of the integrator is operably connected to an ignition
25 charge pulse and the ionization signal input of the
integrator is operably connected to an ionization current
measuring circuit.

Further scope of applicability of the present invention will
30 become apparent from the following detailed description,
claims, and drawings. However, it should be understood that
the detailed description and specific examples, while

indicating preferred embodiments of the invention, are given by way of illustration only, since various changes and modifications within the scope of the invention as defined by the appended claims.

5

Brief Description of the Drawings

The invention will now be further described by way of example only, with reference to the accompanying drawings, in which:

10

Figure 1 is an electrical schematic of a circuit for measuring ionization current in a combustion chamber of an internal combustion engine;

15

Figure 2 is a graph of an ionization signal;

Figure 3 illustrates a production ionization current detection setup;

20

Figure 4a is a plot of an ionization signal for a closed secondary winding;

Figure 4b is a plot of an ionization signal for an open secondary winding;

25

Figure 5 illustrates a comparison of the normalized integrated values of normal and open secondary conditions with different charge durations;

30

Figure 6 a logic block diagram of the open secondary detection apparatus which integrates spark energy;

Figure 7 is a flowchart of the steps taken in determining whether there is an open secondary winding by integrating spark energy;

5 Figure 8 a logic block diagram of the open secondary detection apparatus which measures spark duration; and

10 Figure 9 is a flowchart of the steps taken in determining whether there is an open secondary winding by measuring spark duration.

Detailed Description of the Preferred Embodiment

15 In a preferred embodiment, the invention comprises two methods of detecting an open-secondary winding 18 using the ionization current 100. The first method measures spark energy and the second measures spark duration.

20 Figure 1 is a basic electrical schematic of a circuit 10 that can be used for measuring ionization current in a combustion chamber of an internal combustion engine. The ionization current measuring circuit 10 includes an ignition coil 12 and an ignition or a spark plug 14 disposed in a combustion chamber of an internal combustion engine. The ignition coil
25 12 includes a primary winding 16 and a secondary winding 18. The ignition plug 14 is connected in electrical series between a first end of the secondary winding 18 and ground potential. The electrical connections to a second end of the secondary winding 18 are described further below. A first end
30 of the primary winding 16 is electrically connected to a positive electrode of a battery 20. A second end of the primary winding 16 is electrically connected to the collector

terminal of an insulated gate bipolar transistor (IGBT) or other type of transistor or switch 22 and a first end of a first resistor 24. The base terminal of the IGBT 22 receives a control signal, labelled V_{IN} in Figure 1, from a powertrain control module (PCM) 95. Control signal V_{IN} gates IGBT 22 on and off, thus charging the primary winding of the ignition coil. When the charge is completed (or in other words, when the IGBT is turned off), the voltage builds up over the secondary winding. If there is a spark plug connected to the secondary winding and the voltage is high enough to jump the spark gap, a spark will be generated between the spark gap. The charged energy produced is then dissipated through the spark current.

A second resistor 25 is electrically connected in series between the emitter terminal of the IGBT 22 and ground. A second end of the first resistor 24 is electrically connected to the anode of a first diode 26. The circuit 10 further includes a capacitor 28. A first end of the capacitor 28 is electrically connected to the cathode of the first diode 26 and a current mirror circuit 30. A second end of the capacitor 28 is grounded. A first Zener diode 32 is electrically connected across or, in other words, in parallel with the capacitor 28 with the cathode of the first Zener diode 32 electrically connected to the first end of the capacitor 28 and the anode of the first Zener diode 32 electrically connected to ground.

The current mirror circuit 30 includes first and second pnp transistors 34 and 36 respectively. The pnp transistors 34 and 36 are matched transistors. The emitter terminals of the pnp transistors 34 and 36 are electrically connected to the

first end of the capacitor 28. The base terminals of the pnp transistors 34 and 36 are electrically connected to each other as well as a first node 38. The collector terminal of the first pnp transistor 34 is also electrically connected to the first node 38, whereby the collector terminal and the base terminal of the first pnp transistor 34 are shorted. Thus, the first pnp transistor 34 functions as a diode. A third resistor 40 is electrically connected in series between the collector terminal of the second pnp transistor 36 and ground.

A second diode 42 is also included in the circuit 10. The cathode of the second diode 42 is electrically connected to the first end of the capacitor 28 and the emitter terminals of the first and second pnp transistors 34 and 36. The anode of the second diode 42 is electrically connected to the first node 38.

The circuit 10 also includes a fourth resistor 44. A first end of the fourth resistor 44 is electrically connected to the first node 38. A second end of the fourth resistor 44 is electrically connected to the second end of the secondary winding 18 (opposite the ignition plug 14) and the cathode of a second Zener diode 46. The anode of the second Zener diode 46 is grounded.

In a spark ignition (SI) engine system, the spark plug 14 already inside of the combustion chamber can be used as a detection device without requiring the intrusion of a separate sensor. During the engine combustion process, a large amount of ions are produced in the plasma. For example, H_3O^+ , $C_3H_3^+$, and CHO^+ are produced by the chemical reactions

at the flame front and have a sufficiently long enough exciting time to be detected. If a voltage is applied across the spark plug gap, these free ions are attracted. As a result of this attraction, an ionization signal 100 is
5 generated.

The spark plug ionization signal 100 measures the local conductivity at the spark plug gap when combustion occurs in the cylinder. The changes of the ionization signal 100 versus
10 crank angle can be related to different stages of a combustion process. The ionization signal 100 typically has two phases: the ignition phase, and the post ignition phase. The ignition phase occurs when the ignition coil 12 is charged and later ignites the air/fuel mixture. The post
15 ignition phase occurs when the flame develops in the cylinder (flame front movement during the flame kernel formation). The present invention uses the ignition phase ionization signal, which provides a saturated ignition current measurement that can be used to detect an open secondary. The ionization
20 current in the post ignition phase has been shown to be strongly related to the minimum timing for the best torque (MBT) ignition timing, the air/fuel ratio, the exhaust gas recirculation (EGR) rate, the peak cylinder pressure location, the burn rate, etc. (The MBT ignition timing is
25 that at which the ignition/spark is timed so that the engine produces its maximum brake torque with a given air to fuel mixture.) Figure 2 shows a plot of an ionization signal or ionization voltage (proportional to ionization current I_{ION}
205) with both charge ignition 141 and post-charge ignition
30 signals 143.

A typical ignition system with ionization detection

capability is shown in Figure 3. The ionization detection setup 80 consists of a coil-on-plug or pencil coil arrangement, with a device in each coil to apply a bias voltage across the tip when the spark is not arcing. The current across the spark plug tip is isolated by a current mirror and amplified prior to being measured. The coils 81 (with ion detection) are attached to a module 82 (with ion processing).

10 The failure of a spark plug 14 to spark is reflected in the ionization signal 100 during its ignition phase 141. As stated earlier, the present invention discloses two open secondary detection methods, an ionization spark energy measurement method and a spark duration measurement method.

15 An open secondary winding 18 can be detected by observing whether a spark occurred. The energy is defined as the ionization voltage 100 during ignition integrated over an ignition window. Typically, the ionization spark energy, which is different from the actual spark energy, can be approximated by using the formula

$$E = \int_0^T V^2_{ION}/R \, dt,$$

25 where E represents energy, V_{ION} represents ionization voltage proportional to ionization current 205, R represents load resistance, and T represents spark duration. In a preferred embodiment, ionization voltage 100 is integrated over the spark window 85 and the integrated energy 87 obtained is compared with a reference or threshold 89. If the integrated energy 87 is less than the threshold 89, then no spark

occurred and the secondary winding 18 is assumed to be open. The spark window 85 is defined as a fixed time duration after charge is completed. In a preferred embodiment, the present ignition system uses a spark window 85 with a width of
5 500 μ s. The spark window 85 size can fall anywhere between 300 μ s and 3 ms, depending on the actual spark duration of the given ignition system. Thus, one advantage of the present invention is that it integrates the ionization voltage 100 or ionization signal 100 over a short spark window, thus
10 reducing processing time.

Since resistance R is assumed to be constant due to the ionization measurement circuit, and it is known that the circuit saturates during a spark event, multiplying V_{MAX}^2
15 (where V_{MAX} is the maximum voltage that an ionization measurement circuit produces) by the spark window time 85 results in a representative integrated energy value 87 or integrated value 87. In order to simplify the integration calculation, instead of integrating the square of the
20 ionization voltage, the ionization voltage 100 is integrated directly. A representative or typical integrated energy value for a cylinder that sparked is $(5V) \cdot 0.5 \text{ ms}$ (assuming the resistor value equal to one), which is approximately proportional to the actual spark energy that is defined by
25 the integration of the product of spark voltage and current over the spark window. The 0.5 ms represents a typical integration window 85 at a typical engine speed (1500 RPM) and load (262 kPa BMEP - Brake Mean Effective Pressure). The actual window varies with engine speed and load. The 5 volts
30 represents the maximum value that the ionization measurement circuit shown in Figure 1 produces. The reference value or threshold energy level 89 is set at 75% of this typical

integrated energy value 87. The actual threshold level 89 could vary between 65 to 85 percent of the typical integrated energy value 87 or integrated value 87. Thus, the threshold 89 is calculated by using a maximum voltage V_{MAX} that an ionization measurement circuit produces, multiplying this maximum voltage V_{MAX} by a spark window time 85, whereby a typical integrated energy value 87 is calculated, and multiplying the integrated energy value 87 by a percentage.

10 In a preferred embodiment, detection of an open secondary 18 occurs during the ignition phase 141 of the ionization signal 100. For an ionization detection system with ionization and ignition or spark current 204 flowing in the same direction (see Figure 1), the mirrored ionization current is proportional to the ignition current 204 during the spark window 85.

Since the ignition current 204 is at a milliamperere level and the ionization current 205 is at the microampere level, the ignition current 204 which is proportional to the ignition phase 141 ionization voltage shown in the ionization signal measurement is often saturated, see Figure 2. The ignition phase 141 ionization voltage shown in Figure 2 consists of two portions, charge current and ignition current. The ramped portion 102 of the signal is proportional to the primary charge current and represents the imposed charge current signal. The pulse 104 represents the saturated ignition current 204 (see Figure 4).

30 Note that there is no ignition current in the case of an open-secondary winding 18. Figure 4 shows a comparison of the ignition phase ionization voltage 100 for the normal

operation (Figure 4a) and with an open secondary 18 (Figure 4b). An ignition current pulse which is proportional to the ignition voltage pulse 104 shown in Figure 4a can be observed for a normal operational conditions, and only a ringing voltage 109 which is proportional to a ringing current can be observed for the open-secondary case (Figure 4b).

Therefore, the proposed method of detecting the open secondary winding 18 is to integrate the ionization voltage 100 over the spark window 85 or integration window 85 and then compare the integrated value 87 with a given threshold energy level 89. If the integrated value 87 is below the threshold 89, then there is an open secondary 18. Threshold 89 can also be a function of engine operational speed, load, etc.

Figure 5 illustrates a comparison of the normalized integrated values 87 of normal and open secondary conditions with different charge durations. There exists a large gap in the integrated values 87 between the case of normal operation and the case of an open secondary. Thus, if the threshold is applied in the middle, see Figure 5, an open secondary can be easily detected even if the dwell durations vary significantly, thus providing another advantage of the present invention. In Figure 5, dwell times vary from 0.6 ms to 1.1 ms.

The open secondary detection apparatus 50 of the present invention uses an integrator 90 to integrate the ionization signal 100, and then use a comparator 92 to determine if the integrated ionization signal over the spark window 85 is above a certain threshold 89. If so, then a spark has

occurred. Otherwise, a spark has failed to occur which indicates that the secondary 18 is open.

Figure 6 is a logic block diagram of the open secondary
5 detection apparatus 50. An overall flowchart showing the
logic used in determining whether there is an open secondary
winding is shown in Figure 7. The open secondary detection
apparatus is enabled by the powertrain control module 95
which sends an open secondary detection enable flag signal 97
10 to the enable input 91 of the integrator 90 (200). When the
apparatus 50 is enabled, the integrator 90 is reset (210). In
a preferred embodiment, a reset pulse sent to the
integrator's 90 reset input 93 resets the integrator 90
before the integration step (see below). Often, the rising
15 edge of the ignition charge pulse V_{IN} (from the powertrain
control module 95) can also be used for the reset step. Next,
the measured ionization signal 100 is detected (215) and
integrated over the spark window 85 (220). Then, the
integrated value 87 is compared with a given threshold 89 (or
20 reference) (230) in the comparator 92. The powertrain control
module 95 queries "is the integrated value 87 greater than
the threshold 89 (235)?" If the answer is no, then the
integrated value 87 is below the threshold 89 and the output
94 of comparator 92 is set to logic "zero" and the powertrain
25 control module 95 sets the open secondary flag 99 (240). If
the answer is yes, then the secondary 18 is not open (245).

The open secondary detection apparatus 60 shown in Figure 8
of the present invention measures spark duration. Open
30 secondary detection apparatus 60 uses a first comparator 110
that compares the ionization signal 100 with a first
threshold 115 over the spark window 85. As long as the

magnitude of the ionization signal 100 is above threshold 115, a control signal 136 enables timer 120. Timer 120 measures the time when the ionization signal 100 is above threshold 115 and outputs an ignition duration signal 125, which is a measure of the ignition duration. Next, ignition duration signal 125 is input into a second comparator 140. Comparator 140 determines if the ignition duration 125 is above a duration second threshold 135. If it is, then a spark has occurred. Otherwise, a spark has failed to occur which indicates that the secondary 18 is open.

Figure 8 is a logic block diagram of the open secondary detection apparatus 60. An overall flowchart showing the logic steps taken in determining whether there is an open secondary winding is shown in Figure 9. The open secondary detection apparatus 60 is enabled by the powertrain control module 95 which sends an open secondary detection enable flag signal 126 to the enable inputs 131, 121 of both timer controller 130 and timer 120 (300). When the apparatus 60 is enabled, timer 120 is reset and the enable state 117 for timer controller 130 is set to 1 (305). In a preferred embodiment, the rising edge of the enable signal can be used for the reset. Next, the measured ionization signal 100 is detected (315) and compared with threshold 115 over the spark window 85 (320) in first comparator 110. Threshold 115 is set to 60 to 90 percent of the maximum ionization voltage which is proportional to the ionization current. In the case where the maximum ionization voltage is 5 volts, the threshold 115 can be set between 3 to 4.5 volts. The comparator queries "Is the ionization signal 100 greater than threshold 115?" (322) If the ionization signal 100 is greater than threshold 115, then the first comparator's 110 output 116 is set to logic

"one" (325). Otherwise output 116 is set to logic "zero" (328).

Output 116 is input to timer controller 130. If output 116 is
5 set to logic "one", which occurs when the magnitude of the
ionization signal 100 is above threshold 115, the timer
controller 130 sets its timer enable flag output 136 to logic
"one" and sets enable state 117 to zero (330). Timer enable
flag output 136 is input to timer 120. Setting timer enable
10 flag to logic "one" starts timer 120 (332). Next, the system
60 queries "Is the ionization signal 100 greater than
threshold 115?" (335) The timer 120 continues to count the
pulse duration as long as the magnitude of the ionization
signal 100 is greater than threshold 115 (337). When the
15 magnitude of the ionization signal 100 falls below the
threshold 115 (338), the first comparator's 110 output 116 is
set to logic "zero" (340) which disables the timer 120. The
timer's 120 output 125 is compared with a second threshold
135 or the time duration threshold 135 in comparator 140. The
20 system 60 queries "is the timer output 125 greater than the
threshold 135?" (342). Threshold 135 is set to 60 to 90
percent of the minimum spark duration of the given ignition
system. For an ignition system with minimal spark duration
equal to 0.3 ms, threshold 140 can be selected between 0.18
25 to 0.27 ms. If the answer is no, then the timer output 125 is
below the threshold 140 and the secondary 18 is open. The
powertrain control module 95 sets the open secondary flag 99
to "Yes" (345). If the answer is yes, then the secondary 18
is not open and the powertrain control module 95 sets the
30 open secondary flag 99 to "No" (350).

While the invention has been disclosed in this patent

application by reference to the details of preferred
embodiments of the invention, it is to be understood that the
disclosure is intended in an illustrative rather than in a
limiting sense, as it is contemplated that modification will
5 readily occur to those skilled in the art, within the scope
of the appended claims.

Claims:

1. A method of detecting an open secondary winding in a motor vehicle spark ignition system, comprising the steps of:
5 enabling an integrator;
 resetting said integrator;
 detecting an ionization voltage;
 integrating said ionization voltage over a spark window;
 comparing said integrated ionization voltage with a
10 threshold; and
 setting an open secondary flag if said integrated ionization voltage is below said threshold.
2. A method of detecting an open secondary winding
15 according to Claim 1, wherein said step of enabling an integrator comprises sending an open secondary detection enable flag signal.
3. A method of detecting an open secondary winding
20 according to Claim 2, further comprising the steps of:
 using a rising edge of an ignition charge pulse to reset said integrator;
 calculating said threshold by
 multiplying a maximum ionization voltage by a spark
25 window time, whereby an integrated value is calculated, and
 multiplying said integrated value by a percentage; and
 wherein a size of said spark window is between 300 μ s and 3 ms, said maximum voltage is 5 V, and a powertrain control module sets said open secondary flag.
- 30 4. A method of detecting an open secondary winding according to any preceding, further comprising a step of

using a rising edge of an ignition charge pulse to reset said integrator.

5. A method of detecting an open secondary winding
5 according to any preceding claim, wherein a size of said spark window is between 300 μ s and 3 ms.

6. A method of detecting an open secondary winding
according to any preceding claim, wherein a powertrain
10 control module sets said open secondary flag.

7. A method of detecting an open secondary winding
according to any preceding claim, further comprising a step
of calculating said threshold by:
15 multiplying a maximum ionization voltage by a spark
window time, whereby an integrated value is calculated, and
multiplying said integrated value by a percentage.

8. The method of detecting an open secondary winding
20 according to claim 6 wherein said percentage is 75%.

9. A method of detecting an open secondary winding
according to any preceding claim, wherein said step of
detecting an open secondary occurs during an ignition phase
25 of an ionization signal.

10. A method of detecting an open secondary winding in a
motor vehicle spark ignition system, comprising the step of
measuring spark duration.

30 11. A method of detecting an open secondary winding
according to Claim 10, wherein said step of measuring spark

duration comprises:

comparing an ionization signal with a first threshold;
measuring the spark duration when said ionization
signal is greater than said first threshold;
5 comparing said spark duration with a second threshold;
and
setting an open secondary flag.

12. The method of detecting an open secondary winding
10 according to Claim 10, wherein said step of measuring spark
duration comprises:

detecting an ionization signal over a spark window;
comparing said ionization signal with a first threshold;
enabling a timer if said detected ionization signal is
15 greater than said first threshold;
disabling said timer after said detected ionization
signal falls below said first threshold;
comparing a timer output with a second threshold; and
setting an open secondary flag if said timer output is
20 below said second threshold.

13. An open secondary winding detection apparatus for a
motor vehicle spark ignition system, comprising:

a first comparator having a first and a second input and
25 an output, wherein said first input is operably connected to
an ionization signal and said second input is operably
connected to a first threshold;

a controller having a first and an enable input and an
output, wherein said first input is operably connected to
30 said output of said first comparator;

a timer having a first and an enable input, and an
output, wherein said first input is operably connected to

said output of said controller; and

a second comparator having a first and a second input and an output, wherein said first input is operably connected to said output of said timer and said second input is
5 operably connected to a second threshold.

14. An open secondary winding detection apparatus according to Claim 13, further comprising a powertrain control module having an output operably connected to said enable input of
10 said controller.

15. An open secondary winding detection apparatus for a motor vehicle spark ignition system, comprising:

an integrator having an ionization signal input, an
15 enable input, a reset input and an output; and

a comparator having a first input operably connected to said output of said integrator, a second input operably connected to a threshold value, and an output.

20 16. An open secondary winding detection apparatus according to Claim 15, further comprising an open secondary detection enable flag signal operably connected to said enable input of said integrator for enabling said enable input.

25 17. An open secondary winding detection apparatus according to Claim 15 or Claim 16, further comprising a powertrain control module having an input operably connected to said output of said comparator and an output operably connected to said enable input of said integrator.

30

18. An open secondary winding detection apparatus according to any of Claims 15 to 17, wherein said reset input of said

integrator is operably connected to an ignition charge pulse.

19. An open secondary winding detection apparatus according to any of Claims 15 to 18, wherein said ionization signal
5 input of said integrator is operably connected to an ionization current measuring circuit.

20. A method of detecting an open secondary winding in a motor vehicle spark ignition system, substantially as herein
10 described, with reference to or as shown in the accompanying drawings.

21. An open secondary winding detection apparatus for a motor vehicle spark ignition system, substantially as herein
15 described, with reference to or as shown in the accompanying drawings.



Application No: GB0418621.9
Claims searched: 1 to 9, 15 to 19

13 Examiner: Catherine Allen
Date of search: 21 December 2004

Patents Act 1977: Search Report under Section 17

Documents considered to be relevant:

Category	Relevant to claims	Identity of document and passage or figure of particular relevance
X	1, 9, 15, 18 & 19	US5054461 A MOTOROLA INC see col 3, line 54 to col 4, line 37 and col 7, lines 33 to 44, and figures 1 and 9
A	-	EP0526219 A2 MOTOROLA INC see col 2 line 56 to col 3, line 6 and col 5, lines 37 to 51
A	-	GB2396186 A VISTEON GLOBAL TECH INC see page 28, lines 11 to 13 and page 30, lines 27 to 33

Categories:

X Document indicating lack of novelty or inventive step	A Document indicating technological background and/or state of the art.
Y Document indicating lack of inventive step if combined with one or more other documents of same category.	P Document published on or after the declared priority date but before the filing date of this invention.
& Member of the same patent family	E Patent document published on or after, but with priority date earlier than, the filing date of this application.

Field of Search:

Search of GB, EP, WO & US patent documents classified in the following areas of the UKC^W :

F1B

Worldwide search of patent documents classified in the following areas of the IPC⁰⁷

F02P

The following online and other databases have been used in the preparation of this search report

EPODOC, JAPIO, WPI